

# Hand-In Exercise: Admittance Controller

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## 1 Admittance Control

Design admittance controllers in operational space with the orientational part expressed a) with quaternion and b) with Euler angles.

### 1.1 Control Law

This section presents the admittance controller, where the translational part of the admittance controller is given by

$$M_p \Delta \ddot{p}_{cd} + D_p \Delta \dot{p}_{cd} + K_p \Delta p_{cd} = f \quad (1)$$

where  $M_p, D_p, K_p$  are  $3 \times 3$  matrices,  $f \in \mathbb{R}^3$  is force given in Base frame, and  $\Delta p_{cd} = p_c - p_d$ .

The rotational part of the admittance controller can be expressed in different ways depending on the representation use for orientation. Two representations are

$$M_o \Delta \dot{\omega}_{cd}^d + D_o \Delta \omega_{cd}^d + K_o' \epsilon_{cd}^d = \mu^d \quad (2)$$

$$M_o \Delta \ddot{\phi}_{cd} + D_o \Delta \dot{\phi}_{cd} + K_o \Delta \phi_{cd} = T^T(\phi_c) \mu \quad (3)$$

where  $M_o, D_o, K_o$  are  $3 \times 3$  matrices,  $\mu^d \in \mathbb{R}^3$  is the torque applied to the end-effector given in desired frame,  $\Delta \omega_{cd} = \omega_c - \omega_d$ ,  $\epsilon_{cd}^d = \eta_d \epsilon_c - \eta_c \epsilon_d - S(\epsilon_c) \epsilon_d$ , and  $\Delta \phi_{cd} = \phi_c - \phi_d$ . The rotational stiffness matrix is

$$K_o' = 2E^T(\eta_{cd}, \epsilon_{cd}^d) K_o$$

where  $K_o$  is the stiffness in Euler angle representation and

$$E(\eta, \epsilon) = \eta I - S(\epsilon)$$

### 1.2 Gain Selection

Write how the gains should be selected to obtain a critically damped system.

The gains should be selected in such a way that the  $M_p, D_p, K_p$  follow the equation:

$$\zeta = \frac{K_D}{2\sqrt{M_p K_p}} \quad (4)$$

$$D_p = 2\sqrt{M_p K_p} \quad (5)$$

where  $\zeta$  is the damping ratio,  $K_d$  is the derivative gain,  $M_p$  is the mass,  $K_p$  is the proportional gain, and  $D_p$  is the damping gain. For a system to be critically damped, the damping ratio  $\zeta$  should be equal to 1.

### 1.3 Implementation

Provide details on the implementation of the controller.

The moment in the desired frame is computed from the wrench  $h_e$  as

$$\mu^d = R_d^e(t)^T \cdot \mu_e + R_d^e(t)^T \cdot S(p_d^e) \cdot f_e \quad (6)$$

where  $h_e = \begin{bmatrix} \mu_e \\ f_e \end{bmatrix}$  is an external wrench applied to the end-effector,  $R_d^e(t)$  is the rotation matrix between the end-effector and the desired frame, and  $p_d^e$  is the position of the desired point relative to the end-effector frame.

#### 1.3.1 Quaternion-Based Controller

The quaternion  $(\eta_{cd}, \epsilon_{cd}^d)$  is obtained from integration of  $\omega_{cd}^d$  as

$$q(t + dt) = \exp\left(\frac{dt}{2} \omega_{cd}^d(t + dt)\right) * q(t) \quad (7)$$

The compliant frame  $p_c$  is obtained from the quaternion  $(\eta_{cd}, \epsilon_{cd}^d)$  as

$$p_c = q_d \cdot q_{cd}^d \quad (8)$$

#### 1.3.2 Euler Angle-Based Controller

The Euler angle  $\Delta\phi_{cd}$  is obtained from integration of  $\Delta\dot{\phi}_{cd}$  as

$$\Delta\phi_{cd} = \int \Delta\dot{\phi}_{cd} dt \quad (9)$$

The compliant frame  $p_c$  is obtained from the Euler angle  $\Delta\phi_{cd}$  as

$$p_c = R_z(\Delta\phi_z) \cdot R_y(\Delta\phi_y) \cdot R_x(\Delta\phi_x) \cdot p \quad (10)$$

where  $\Delta\phi_{cd} = (\Delta\phi_x, \Delta\phi_y, \Delta\phi_z)$

## 2 Simulation

Insert simulation results for the admittance controlled robot. The admittance controller should have a desired motion of your choice. In addition, no external force should be applied for the first five seconds, then a force  $f = (1, 2, 3)$  N should be added for five seconds, then no external force for five seconds, then a torque  $\mu = (1, 0.5, 1)$  Nm for five seconds and lastly no external force for five seconds. You should include figures that documents the simulation including applied wrench, desired motion, actual motion.

The desired motion is:

$$\begin{aligned} x_{\text{ref}}(t) &= 0.3 \sin\left(\frac{t}{3}\right), \\ y_{\text{ref}}(t) &= 0.3 \sin\left(\frac{t}{3}\right) \cos\left(\frac{t}{3}\right), \\ z_{\text{ref}}(t) &= 0.1 \sin(t), \\ q_{\text{ref}}(t) &= 1, \end{aligned}$$

and is plotted on Figure 4.

The robot should be controlled in the following compliance frame:

$$T_c^s = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0.1 \\ 0 & 0 & 1 & 0.2 \\ 0 & 0 & 0 & 1 \end{bmatrix}.$$

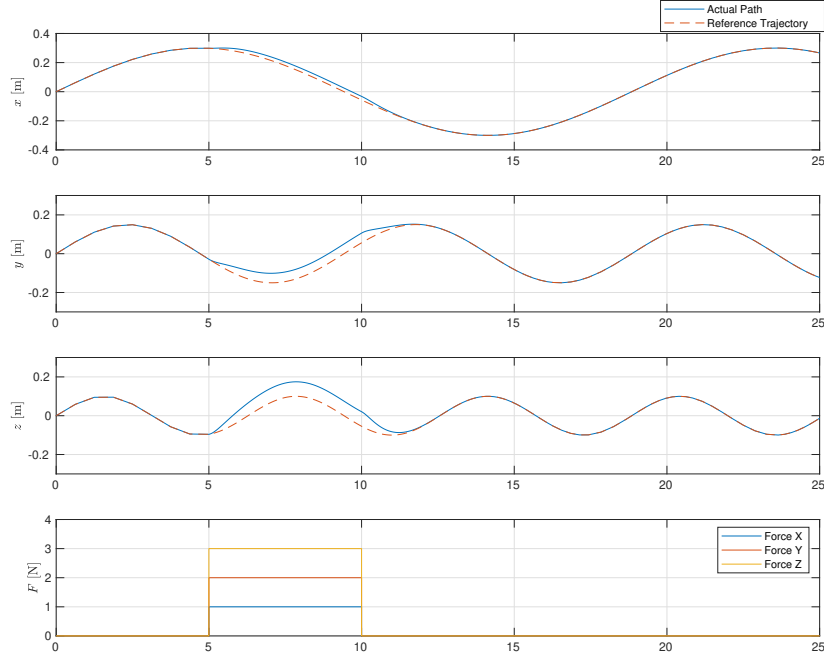


Figure 1: Desired motion, actual motion and applied forces vs time

where  $K_p=40$ ,  $M=5$  kg, initial pose and velocity are 0.

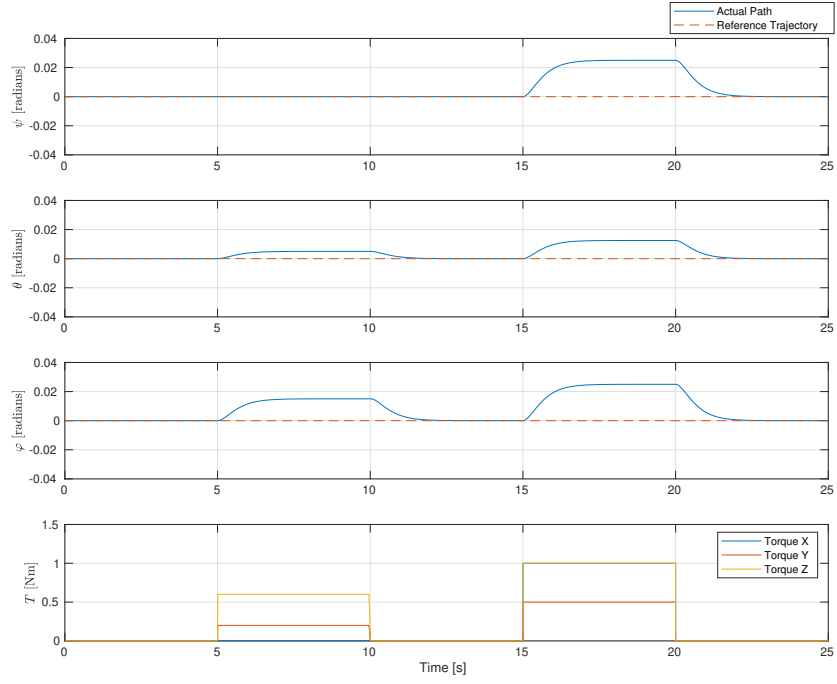


Figure 2: Desired angular motion, actual angular motion in Euler angles and applied torques vs time

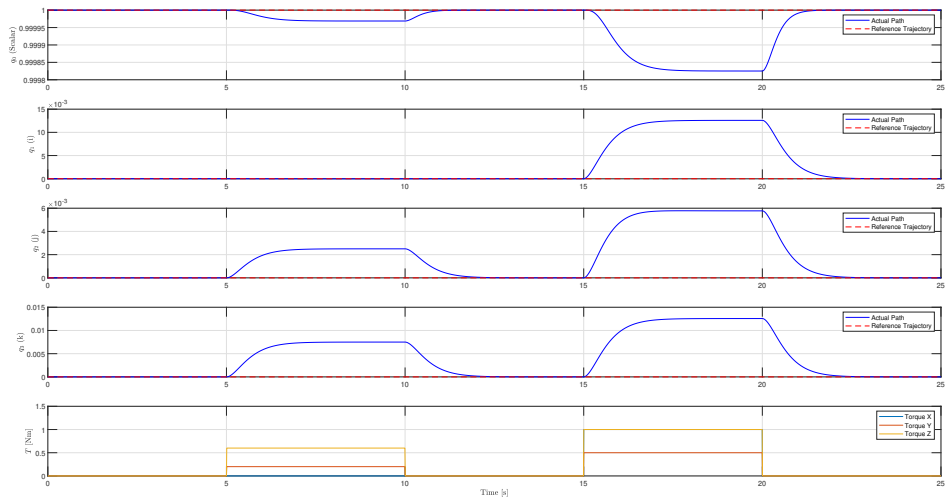


Figure 3: Desired angular motion, actual angular motion in quaternions and applied torques vs time

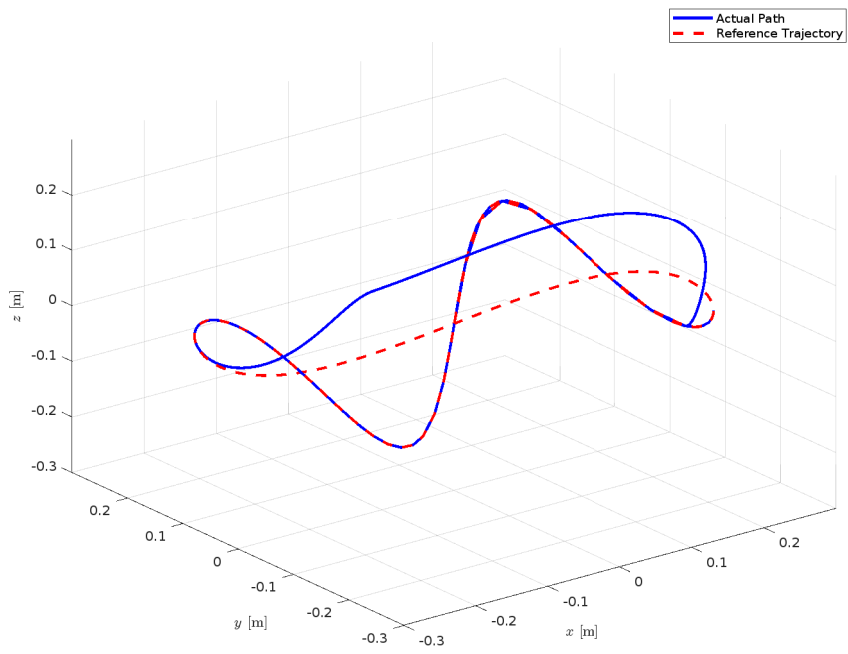


Figure 4: 3D representation of the translational motion of the robot